Comparison of Howland and General Impedance Converter (GIC) circuit based current sources for bio-impedance measurements

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Comparison of Howland and General Impedance Converter (GIC) circuit based current sources for bio-impedance measurements

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Abstract: The current source is a key component in bio-impedance measurement systems. The accuracy of the current source can be measured in terms of its output impedance together with other parameters, with certain applications demanding extremely high output impedance. This paper presents an investigation and comparison of different current source designs based on the Enhanced Howland circuit combined with a General Impedance Converter (GIC) circuit using both ideal and non-ideal operational amplifiers. Under differing load conditions two different settings of the GIC are evaluated and the results are compared to show its performance settings. Whilst the study has shown that over a wide bandwidth (i.e. 100Hz – 100MHz) the output impedance is limited, operation over a more limited range offers output impedance in the Giga-ohm range, which can be considered as being infinite.

1. Introduction

In any bio-impedance measurement system, unknown impedance can be measured by two possible methods: either by the application of a known voltage across the subject, and then measuring the current through it, or by injecting a known current into the subject and measuring the voltage across it. Unknown contact impedance exists between the electrode and the subject. It will degrade the operation of voltage source having low output impedance. Therefore we must preferably use the second method – to inject current and measure voltage across the object [1].

An important parameter of a current source is its output impedance which is frequency dependent. Ideally the output impedance should be infinitely large; so primarily this paper will investigate ways to achieve the highest possible value of output impedance of current source. Bandwidth of the current source is also an important factor. EIT systems require a wide range of frequencies. Apart from output impedance this paper will also investigate the bandwidth of current source under different loads.

The current source which is mostly used in bio-impedance measuring systems is the Enhanced Howland circuit. According to the available literature [2] [3], the Enhanced Howland circuit has limited output impedance which is consistent across a wide bandwidth. At higher frequencies, the output impedance degrades due to the presence of output capacitance and by cancelling this output capacitance higher output impedance can be achieved. The placement of a GIC in parallel with an Enhanced Howland circuit is known to improve the output impedance of the circuit [4].

In this paper, the Enhanced Howland-GIC circuit is simulated with ideal and non-ideal operational amplifiers. This paper is a comparison and simulation of the Enhanced Howland-GIC circuit with...
different devices currently available in the market to find the theoretically maximum achievable output impedance. To reduce the output capacitance of the system, different settings of the GIC are simulated, and its output impedance and bandwidth performance are established.

2. Current Source Architecture

2.1. Enhanced Howland Circuit
To remove the common mode voltage or Loading effects in the Basic Howland circuit a resistor is added between the non-inverting and the output terminals to improve the performance of the circuit (see fig. 1). This Enhanced Howland circuit is used as a current source in most EIT systems due to its simple architecture and better performance [1][2][3][5][6]. In terms of output impedance, the Enhanced Howland circuit does not give our desired high output impedance due to the presence of output capacitance. The Output current of the Enhanced Howland circuit for an ideal op amp is given as,

\[
I = V' \left( \frac{R_2}{R_1} + \frac{R_4}{R_1 \cdot (R_5 + R_2)} \left( \frac{R_2}{R_1} + \frac{R_3}{R_2} \right) \right)
\]

(1)

2.2. Generalized Impedance converter (GIC)
GIC circuit is from Northrop [7]. It consists of two operational amplifiers and five discrete components which can be used to synthesize various impedances. These components are either resistors or capacitors. There are several topologies to implement this circuit. In our case, we want to cancel the output capacitance of the current source circuit by configuring the GIC to effectively produce inductance. Therefore, for inductive output the GIC should have two operational amplifiers, four resistors and one capacitor [7]. The inductance produced will have the value:

\[
L = \frac{R_1 R_3 R_5 C_2}{R_4}
\]

(2)

\[
L = \frac{R_1 R_3 R_5 C_4}{R_2}
\]

(3)

3. Methodologies
A GIC circuit is placed in parallel with Enhanced Howland circuit for output capacitance cancellation as shown in figure 1. The circuit is simulated using PSpice over a wide range of frequencies i.e. up to 1GHz. Output impedance of the circuit is calculated up to 10MHz over different loads i.e. 1k, 2k, 4k, 10k, 20k, 40k. Initially, the Enhanced Howland-GIC circuit is tuned to a single resistor and capacitor setting to achieve maximum possible performance with a single configuration. It is noticed that this configuration will have high output impedance at lower frequencies but the output capacitance degrades the performance at higher frequencies. On the other hand, it covers a wide range of frequencies, as defined by the amplifier bandwidth specifications. This design is called the single network configuration (see figure 2).

The Enhanced Howland-GIC circuit can also be tuned to achieve higher output impedance, but over a limited frequency range. This kind of design we have named multiple network configuration (see figure 3 for a 1MHz spot frequency performance).
4. Results and Discussion
The circuit was simulated using an ideal operational amplifier present in PSpice libraries. This paper gives simulation results to show maximum output impedance achieved from group of selectable devices. Either 2nd or 4th component in GIC can be a capacitor. In this paper we had placed capacitor at both location and have noticed its results.
Non-ideal operational amplifiers (OPA656, THS4304 and THS3201 by Texas Instruments and AD8055 by Analog Devices) are simulated using single & multiple circuit configurations as well as different capacitor configurations. These operational amplifiers are selected due to wide bandwidth, higher slew rate, low distortion and simple pin configuration. Table 1 shows the maximum output impedance achieved from all selected non-ideal devices at a particular frequency. e.g. Table 1 shows that maximum output impedance of 4G\(\Omega\) at 100Hz is achieved using OPA656 device for 2nd position of capacitor, while at same frequency 26G\(\Omega\) output impedance is achieved using AD8055 for 4th position of capacitor. This difference in output impedance is due to characteristics of operational amplifier used and tuning of GIC until we achieve maximum current injection. Using single network configuration gives us better bandwidth but the output impedance decreases at 1MHz and above. Table 1 shows the output impedance achieved using different non-ideal amplifiers. Multiple circuit configurations can be used to achieve high output impedance at higher frequencies. Both possible capacitor settings highlighted in figure 1 can be individually used because the system is tuned for very narrow frequency bands at which we achieve maximum current injection. Table 2 shows the output impedance possible using non-ideal amplifiers.
For single network configuration, there is also some phase difference between the load voltage and input voltage. From 100Hz to 100kHz phase difference is 180\(^\circ\). Above 1MHz, phase difference increases and the maximum phase difference at 40k load is 259\(^\circ\). For multiple network configurations, phase difference is 180\(^\circ\) at 1MHz. When this design is implemented in practice, the phase differences introduced need to be taken into consideration during reconstruction, or calibrated out of the measurements.

5. Conclusion
In this paper, Enhanced Howland-GIC circuit has been simulated using ideal and non-ideal operational amplifiers. Both possible capacitor positions in GIC circuit are simulated. Two different configurations are discussed to cover maximum number of frequencies. Multiple network configurations can be helpful to achieve higher output impedance at higher frequencies, tuned to a narrow band. Results show that, most non-ideal devices can give an acceptable level of output impedance, but THS3201 only achieves low output impedance. However, this same device gives
better bandwidth as compared its counterparts. If we want to achieve higher output impedance (i.e. in the GΩ range) with a single configuration at higher frequencies (i.e. > 1MHz), then we have to sacrifice circuit bandwidth.

As mentioned earlier, this paper only gives the simulation results to find maximum achievable output impedance from a specific group of devices while ignoring the parasitic effect of cables, capacitors, resistor, inductor etc. Once the device which gives acceptable output impedance is decided, this circuit will be simulated including the parasitic effects and will be tested practically. These approaches can further be improved using better operational amplifiers when available.

Table 1: Enhanced Howland-GIC output using the single network configuration at different loads

<table>
<thead>
<tr>
<th>Frequency (Hz)</th>
<th>Ideal</th>
<th>Non Ideal (OPA656, THS4304, THS3201, AD8055)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Using capacitor on 2nd Position</td>
<td>Using capacitor on 4th Position</td>
</tr>
<tr>
<td></td>
<td>Max Zo &amp; Corresponding Load</td>
<td>10k Load</td>
</tr>
<tr>
<td>100</td>
<td>6.25G</td>
<td>16.66G</td>
</tr>
<tr>
<td>10k</td>
<td>33G</td>
<td>33G</td>
</tr>
<tr>
<td>100k</td>
<td>33G</td>
<td>33G</td>
</tr>
<tr>
<td>1M</td>
<td>33G</td>
<td>33G</td>
</tr>
<tr>
<td>5M</td>
<td>33G</td>
<td>33G</td>
</tr>
<tr>
<td>10M</td>
<td>33G</td>
<td>33G</td>
</tr>
</tbody>
</table>

Table 2: Enhanced Howland-GIC output using multiple network configurations at different loads

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<th>Frequency (Hz)</th>
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<th>Non Ideal (OPA656, THS4304, THS3201, AD8055)</th>
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References

Hardware System PhD Thesis, De Montfort University, UK